

## STUDY OF BEHBAHAN CITY VELOCITY WAVES SHEAR

SY Zolfegharifar<sup>1,2</sup>, M Bosak<sup>2</sup><sup>1</sup>Department of Geotechnics & Transportation, Faculty of Civil Engineering, Universiti Teknologi Malaysia, MALAYSIA<sup>2</sup>Department of Civil Engineering, Yasooj Branch, Islamic Azad University, Yasooj, IRAN

## ABSTRACT

Behbahan town as one of the important cities of Khuzestan province located in oil reservoirs range and power transfer lines because of sitting in boundary under the making –land units and zagrosprehole at front fault side of mountain that caused heavy earthy uakes with it is movement and also existence of occurousareas.study of previous earth quakes shows that local geology situations ,soil,sediments,and aerobic rocks on bed rock cause aggration of land movements arising of earthquake and it can be said that most importandfactorin final control of area earth quake to structure is building characteristics.sectional waves is animportand extraordinary property of soil which is strongly related to soil dynamic and trembling geoTechnic phenomenons and land movement that is caused by earthquake is by reason of sectional-waves spreading from rock bed towards soil upper layers,that ,irtum cause sectional trans formation along spreading.For acquisition to this assessment,different geotechnical and geology in formation related to Behbahan city Is collected and sectional waves rate is computed bypre send empirical relations

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## KEY WORDS

earth, quake,land-making,  
trmbling,bulding,stanard  
penetration number,sectional

\*Corresponding author:Email:yzfsayyed2@live.utm.my;Tel: +989013617474; Fax:+987433313212

## INTRODUCTION

Earth movements which caused by earth quake is because of sectional waves dispersion from bed rock toward upper layers[1].to do widening carefully, we should spend much expenses to do special actions such as sounding about different limitations specially its financial costs, possibility of new soun ding did not exist in studied area and for knowledge of geo technical situation, we take action to collect results of accomplished laboratorial or open-air tests in considered erea, it is used governmental or private institutions geo technical reports such as accomplished studies for different projects like construction of residential buildings, determining under-ground water and ect. By reason of not being geo technical sunding, it is tried touse accomplished studies by oil companies located around Behbahan city ti achieve mire exact in formation from soil layers han profile. thus, researches data are used in analyze of soil layers response in earth quake interval resarch about 16 geotechnical sounding and wet is stusied, and these soundings involve different brigade to 20 meters depth map of geo technical sondding place is shown in figure1.of course, there are remarks in clarifying some of place geotechnical featurers that we will point them in next section. Dependingon extent of needed information ,degree of earth quake danger widening is divided in to less care arena(Grade-1),mean care(Grade-2)and muchcare (Grade-3) [2].Forlitttle care widening basedon survey present data from damages resulting of past earth quakes, special information arena has little cost care.in mean care arena, much more geotechnical in formation is required them methods with little care and so necessary time and cost to do these studies compared to little care studies, is more.al o ,we can use geotechnical reports of private and governmental (teoropen-air test results in considered area.for much care (Grade-3) geotechnical ex cavations, to accomplishentrtion Tests(CPT-SPT),sampling soil for laboratorial tests, geotechnical ways and collecting present in formation. From erea is necessary. expenses of this kind of earth quake danger widning is much,but exact widning is justifiable for places involovinghigt earth quake danger potential,and vital and sensitive present facilities and future of geotchical studies in behbahan city is sectional wave rate determination with least cost and make studies in shortest time,flattenig care with attention to quality ,and extend present and collected information ,is considered mean care.summary of gotechnicstuy results as sample for 1,2 and 16 sounding is presented in [Figure-1] .

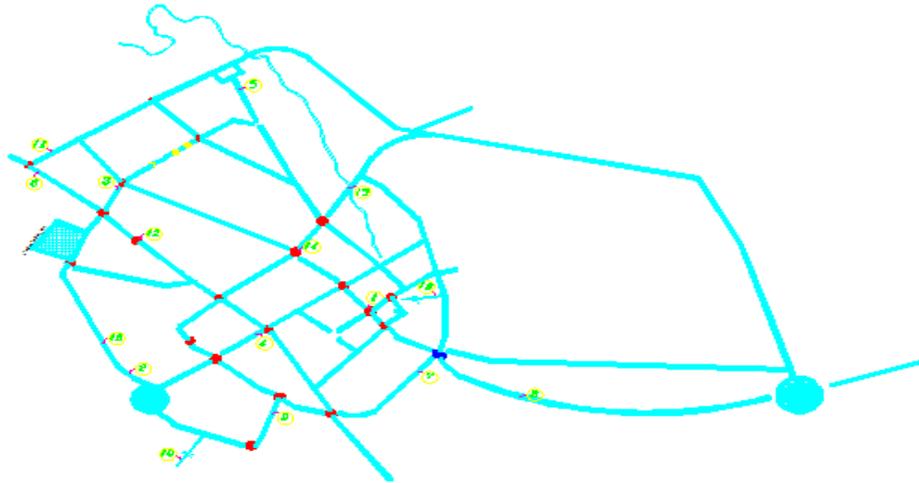


Fig: 1. Place and number of sample geotechnical sounds in present study

## MATERIALS AND METHODS

### Geotechnical remarks of studied place

In [Table-1] with attention to excavation high costs for exact determination of behavior alluvium thickness, it is tried to collect information in this field. Attained information from oil company and water and sewage organization, Maron dam and also study of geology maps shows that behavior soil thickness is 250 to 35 meters.

2.2. Mass,  $\rho_s = 1/95 \text{ g/cm}^3$ . Of course, it is tried that in every sounding analysis, for 20 meter depths downward, SPT number to ascertain sectional wave rate estimated based upper layers of same sounding. Because of that special weight change has not much effect on analyzing layers, special mass of soil with fixed extent,  $\rho_s = 1/95$ , in depths under 20 meters is supposed for all soundings.

measured number SPT in geotechnical studies is measured in terms of N<sub>10</sub> (penetration number based standard energy ratio 10%). Numbers in presence under ground water for depths under 15 meters with assumption that SPT number of these depth measures based on SPT number upper layers, for  $N > 15$  adjust in form of  $N = N - 15(N - 15)$  (there is not sounding for number 1, 2).

Table:1. Summary of granular test results,  $e$ ,  $e_r$ ,  $e_g$  limits, moisture percentage and standard penetration number.

Borehole	Dep	w %	LL %	PI %	SPT	$\rho_w$	USCS
1	0-2	30	-	-	13	1.83	-
	2-4	-	23	7	50	2.2	GC-GM
	4-6	9.1	26	10	28	1.95	CL
	6-10	28	25	9	85	2	CL
	10-13	-	25	8	50	1.98	CL
	13-16	-	28	12	70	2	CL
2	0-3	28	25	10	50/11	1.85	CL
	3-6	28	23	7	50/15	1.85	CL-ML
	6-10	28	24	8	50/9	1.85	CL
	10-16	-	26	10	50	1.85	CL
	16-20	-	-	-	50	1.98	CL
16	0-1	-	-	-	13	1.83	CL
	1-3	8.3	36	15	13	1.67	CL
	3-4	10.6	34	15	13	1.69	CL
	4-5	10.6	34	15	14	1.71	CL
	5-6	16	34	14	14	1.75	CL
	6-8	22.7	33	13	14	1.87	CL
	8-14	-	-	10	14	1.95	CL

## RESULTS

### Correlation between sectional wave rate (vs) and spt number

Earth tremblings that caused by earth quake is because of spreading swares that are known as sectional waves, cause sectional trans formation along spreading [2].with attention to particles Trembling direction,sectional waves are divided into two elements SV(movement in vertical surface) ,SH(movement in horizontalsurface. Sectional waves is an extra or denary property that is strongly related to soil dynamic phenomenon's and trembling geoterch nicetoday ,to determine sectional wave rate for soil layers that is one of the important parameters in addition to object module G<sub>s</sub>,we can act in two ways:1-tests with little tension ,2-tests with high tension. Tests with low tension(tremblinggeophysics tests)usually act in tension rageswitch are not they are mostly in congestion under 0/001%Because of this ,most of them are wave spreading based theory in linear materials.most of them are related to measurement of volume waves rate that are easily connectable with soil module in coge.since,most sectional,conge,trembling geophysical tests produce less than 0/0003%measured sectional wave rates are usable for computationG<sub>max</sub>[1]:

$$G_{max} = \rho v_s^2 \tag{1}$$

using measured sectinal wave rates,are usually most reliable way to measure open-air numbers G<sub>max</sub> for a special layer of soil and trembling geophysic tests are usually used for this .for tedts of which present conge is less than 0/0001 such as open-air trembling tests G,result of tests is G<sub>max</sub>.highcongesation test are most common type formesuring conge properties abov soils such as resistance.so,their result is also connected tration test (spt) is oldest and most common open-air test geotechnicaplications.Number SPT is number of standard hammer strokes invilvin 64kg weght that is necessary for penetration 30 cm from standard to-floor tube spt in to soil.spt number is used for different aims such as internal friction angle  $\theta$  and special weigt for soily.so modification is made to lessen error.inherentsuchasG<sub>max</sub> with penetration parmeterswich are relevant to more much conges,from in formation variance that take action according them,and also from attained results changes by different researchers.because of this ,utility of such relations is limitd to primary estimation G<sub>max</sub>[3].it is suggested some rempirical relations among vs and SPTnumbr.witch some of them is explainable as following:with city ,an cheapier method to determine sectional wave rate by helping .sorrelation bed ween sectional wave rate and number of standard penetration strokes (SPT)is presented.Yapaneseresearchaerli(1992)[4]:

$$V_s = 82.8(N^{0.134})(D+1)^{0.225} \tag{2}$$

$$V_s = 84.5(N^{0.118})(D+1)^{0.236} \tag{3}$$

where D is considered layer and Nis standard penetration.

Relations(2) and(3) are forcl and ml/cl soils.

Hardian and richart (1963),reported obtained results from intensification column on otava dry sand.in these equations,vs is related to porosity ratio and applied effective pressure and explain as following [1].

$$V_s = (19.7 - 9.06e) \sigma_0'^{0.25} \quad \sigma_0' \geq 95.8 \text{ KN / m}^2 \tag{4}$$

$$V_s = (11.36 - 5.35e) \sigma_0'^{0.3} \quad \sigma_0' < 95.8 \text{ KN / m}^2 \tag{5}$$

In above equations,v<sub>s</sub>and  $\sigma_0'$ units are orderly interms of m/S and N/M<sup>2</sup>. 60 average of lateral effective pressure

equals with octahedral effective tension  $\sigma_o' = \frac{1}{3}(\sigma_1' + \sigma_2' + \sigma_3')$  which in that  $\sigma_1', \sigma_2', \sigma_3'$  are oredrlyminimum ,mean and maximum main efective tension of soil.Harian and richart suggested following redationbasdon different tests of grain soils.

$$V_s = (18.43 - 6.2e) \sigma_0'^{0.25} \tag{6}$$

Schmertmann(1978)msuggestedfollowing relation forsand:

$$V_s = 10 \text{ to } 20 N_{60} \tag{7}$$

Seed etal(1986),and later,jamilkowski(1978),presented an approximate relation for sectional wavesrate of different soils.

$$V_s = C_1 N_{60}^{0.17} Z^{0.2} F_1 F_2 \tag{8}$$

C<sub>1</sub>=said and colleaqs,jamiolkwskietal suggested 69 and 53/50

Z=dephwherespt number is obtained for 60%entergy and is intermsofm.

$F_1$ -is age parameter,for alluvium deposit and old alluvium deposit is 1 and 1/3,respectively.  
 $F_2$ -is determinaed for every kind of soil with regarding to following [Table-2]:

Table: 2.show kind of soil

	Clay	Fine sand	Med sand	Coarse sand	Sand & Gravel	Gravel
$F_2$	1.0	1.09	1.07	1.11	1.15	1.45

Yoshidetal (1988),presented following relating for different soils[5].

$$V_s = C_1(\gamma z)^{0.14} N_{60}^{0.25} \tag{9}$$

where  $\gamma z$ =mean pressure and load in depth z intermsofKPa.

$C_1$ -is determined for every kind soil with attention to below [Table-3]

Table: 3. Show kind of soil

Soil	Fine sand	25% gravel	50% gravel	All soils
$C_1$	49	56	60	55

Bazeyar and coworkers presented following relation for iran soil ( $N \leq 50$ )

$$V_s = 134D^{0.12} N^{0.53} \tag{10}$$

Where D is considered layer depth ,nis standard penetration.

Jafari and coworkers presented following relation for Tehran soil

$$V_s = 100N^{0.53} \tag{11} \quad v_s = 43/3 N^{0.03} \tag{12}$$

(11)and(12) relations is for non-adhesive and adhesive soils, respectively.

Toniuchi(1982),Imai presented following relation for large-grain soils [5]:

$$V_s = 75.4N_{67}^{0.351} \tag{13}$$

Go to and ohta (1978)suggestedfollowing relation[5]:

$$V_s = 94.2N_{67}^{0.34} \tag{14}$$

this relation along with relations (15),(16),(17),(18) are relations that present secional wave rate vs h terms of nor spt for different soils:

All types of soils  $V_s = 85.34N^{0.348} \tag{15}$

Clay  $V_s = 85.6N^{0.34} \tag{16}$

Sand  $V_s = 81.32N^{0.34} \tag{17}$

Gravel  $V_s = 104.6N^{0.34} \tag{18}$

## DISCUSSION

In addition to above cases,sectional wave rate vs inter ms of soil depth H is presnted for different types of soil[6]:

$$V_s = 92.12H^{0.339} \tag{19}$$

$$V_s = 78.98H^{0.312} \tag{20}$$

$$V_s = 78.98H^{0.312} \tag{21}$$

$$V_s = 178.1H^{0.312} \tag{22}$$

Relations(19)to(21)are for ;all types of soil ,clay ,standard Gravel soils,respectively.

In all relations,sectional wave rate is in terms of (m/s) and his interms of(m).

By placing relations (15)with(19),(16) wih(20),(17)with(21)and (18) with(22),following relations is achieved between H and N.

$$N = 1.244H^{0.974} \tag{23}$$

$$N = 0.789H^{0.918} \tag{24}$$

$$N = 1.905H^{0.918} \tag{25}$$

$$N = 4.784H^{0.918} \tag{26}$$

We can use relations (23) to (26) for places that (N)SPT is not clear in soil depths.

(26) relation and formula based on type, depth, SPT number and soil geology period is presented in different forms which fitting to changes in these parameters, sectional wave rate of soil layers is identified. As we can observe, most of these relations are presented by Japanese. Because of that obtained relations are more consistent with Japanese soil and geology situation, it is not used relations 15 to 26. Relations 11 and 12 which are special to Tehran soil are not used. In [Table-4] relation B to H are used for computing sectional wave rate of clay soil and relations I to S are used for computing sectional waves in large-grain soils. Relations A and I are used for both soils. Relations T to W are special for sand soils.

**Table:4. Presented relations for determining sectional wave of behbahan soil**

NO.	SOURCE	RELATIONSHIP
A		$G_{max} = \rho v_s^2$
B	Lee (1992)	$V_s = 82.8(N^{0.134})(D+1)^{0.223}$
C	Lee (1992)	$V_s = 84.5(N^{0.118})(D+1)^{0.246}$
D	Seed et al (1986)	$V_s = 69N_{60}^{0.17} Z^{0.2} \times 1 \times 1$
E	Seed et al (1986)	$V_s = 69N_{60}^{0.17} Z^{0.2} \times 1 \times 1 \times 1.3$
F	Jamiolkowski et al (1978)	$V_s = 53.5N_{60}^{0.17} Z^{0.2} \times 1 \times 1$
G	Jamiolkowski et al (1978)	$V_s = 53.5N_{60}^{0.17} Z^{0.2} \times 1 \times 1 \times 1.3$
H	Yoshid et al (1988)	$V_s = 55(\gamma z)^{0.14} N_{60}^{0.25}$
I	Bazryar et al	$V_s = 134D^{0.2} N^{0.1}$
J	Seed et al (1986)	$V_s = 69N_{60}^{0.17} Z^{0.2} \times 1.45 \times 1$
K	Seed et al (1986)	$V_s = 69N_{60}^{0.17} Z^{0.2} \times 1.45 \times 1.3$
L	Jamiolkowski et al (1978)	$V_s = 53.5N_{60}^{0.17} Z^{0.2} \times 1.45 \times 1$
M	Jamiolkowski et al (1978)	$V_s = 53.5N_{60}^{0.17} Z^{0.2} \times 1.45 \times 1.3$
N	Tonouchi (1982) and Lmai	$V_s = 75.4N_{60}^{0.151}$
O	Ohta & Goto (1978)	$V_s = 94.2N_{60}^{0.34}$
P	Yoshid et al (1988)	$V_s = 60(\gamma z)^{0.14} N_{60}^{0.25}$
Q	Hardin, B. O., and	$V_s = (18.43 - 6.2e) \sigma_0^{0.25}$
R	Richart, F. E., Jr. (1963).	$V_s = (11.36 - 5.35e) \sigma_0^{0.3}$
S		$V_s = (19.7 - 9.06e) \sigma_0^{0.25}$
T	Seed et al (1986)	$V_s = 69N_{60}^{0.17} Z^{0.2} \times 1 \times 1.07$
U	Seed et al (1986)	$V_s = 69N_{60}^{0.17} Z^{0.2} \times 1.3 \times 1.07$
V	Jamiolkowski et al (1978)	$V_s = 53.5N_{60}^{0.17} Z^{0.2} \times 1 \times 1.07$
W	Jamiolkowski et al (1978)	$V_s = 53.5N_{60}^{0.17} Z^{0.2} \times 1.3 \times 1.07$

## CONCLUSION

When diffused volume waves resultantly fault break arrive in land between different geology materials, they reflect and refract. While waves spreading rate in less depth materials is generally less than materials under them, arieted rays that encounter with horizontal layer from tier. Usually reflect in more vortical direction. When waves arrive earth surface, their numerous refractions cause their direction to be perpendicular to earth surface. One of the important parameters in trembling geotechnic computer program and one dimension earth reply, is sectional wave rate by two ways. Firstly, sectional wave rate is directly determined by using trembling ways. In second way, sectional rate of soil layers is determined by use of empirical relations between sectional wave rate vs and number of standard penetration test strokes spt. Because of that first method is expensive, second way is mostly used. In second way, sectional wave rate of soil layers is determined based on test result spt and by present empirical relations between spt, some of effective factors in determining these relations are geology age effects, depth and soil type. In this research, many relations are used to determine sectional wave rate, but best relation which was consistent with our region is selected and average is achieved. Also, new relations based on present relations for places where has not spt number or there is in low depth present by author. It should be mentioned that this type of relation studied area, so they are not without error.

## CONFLICT OF INTEREST

None

## ACKNOWLEDGEMENT

None

## FINANCIAL DISCLOSURE

None

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